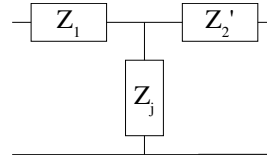
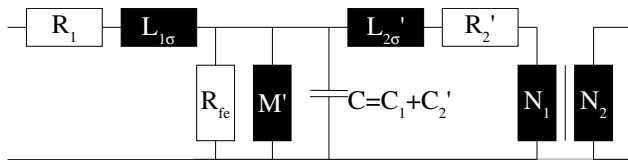


Transformator



$$Z_1 = R_1 + j\omega L_{1\sigma}$$

$$Z_2' = R_2' + j\omega L_{2\sigma}'$$

$$Z_j = R_{fe} \parallel j\omega M' \parallel (j\omega C)^{-1}$$

Vierpolparameter

$$z_{11} = Z_1 + Z_j \quad z_{12} = \frac{Z_j}{\ddot{u}} \quad z_{21} = \frac{Z_j}{\ddot{u}} \quad z_{22} = \frac{Z_2' + Z_j}{\ddot{u}^2} = Z_2 + \frac{Z_j}{\ddot{u}^2}$$

$$z_{11} = Z_1 + Z_j \quad z_{12} = Z_j \quad z_{21} = Z_j \quad z_{22} = Z_2 + Z_j$$

Projektion der Sekundärgrößen auf die Primärseite

$$u' = \ddot{u} u \quad i' = \frac{i}{\ddot{u}}$$

$$Z' = \ddot{u}^2 Z \quad R' = \ddot{u}^2 R \quad L' = \ddot{u}^2 L \quad C' = \frac{C}{\ddot{u}^2}$$

$$u_1 = L_1 \dot{i}_1 + M \dot{i}_2 \quad u_2 = L_2 \dot{i}_2 + M \dot{i}_1$$

Übersetzungsverhältnis

$$\ddot{u} = \frac{N_1}{N_2} = \frac{u_1}{u_2} = -\frac{i_2}{i_1}$$

Kopplungsgrad

$$k = \sqrt{\frac{\Phi_1}{\Phi_2} \frac{h}{\phi_1} \frac{h}{\phi_2}} = \sqrt{L_1 \frac{h}{L_1} L_2 \frac{h}{L_2}} = \frac{M}{\sqrt{L_1 L_2}}$$

Gegeninduktivität

$$M = \ddot{u} L_2 h = L_1 \frac{h}{\ddot{u}} = \frac{N_1 N_2}{R_m} = N_2 \Phi_1 \frac{h}{i_1} = N_1 \Phi_2 \frac{h}{i_2} = k \sqrt{L_1 L_2} = \sqrt{L_1 h L_2 h}$$

$$M' = \ddot{u} M$$

Schwingkreise

Resonanzfrequenz

$$\omega_0 = \frac{1}{\sqrt{LC}} = 2\pi f_0$$

Verstimmung

$$v = \frac{\omega}{\omega_0} - \frac{\omega_0}{\omega}$$

Dämpfung/normierte Bandbreite

$$\Delta\Omega = \frac{1}{Q} = \frac{\Delta\omega}{\omega_0} = \frac{\Delta f}{f_0}$$

Seriell

$$Z = R + j\left(\omega L - \frac{1}{\omega C}\right)$$

Impedanz

Parallel

$$Y = G + j\left(\omega C - \frac{1}{\omega L}\right)$$

Admittanz

$$Z_k = \omega_0 L = \frac{1}{\omega_0 C} = \sqrt{\frac{L}{C}} = \frac{1}{Y_k}$$

Kennwiderstand

$$Y_k = \omega_0 C = \frac{1}{\omega_0 L} = \sqrt{\frac{C}{L}} = \frac{1}{Z_k}$$

Kennleitwert

$$\frac{Z}{R} = 1 + j \frac{Z_k}{R} v = 1 + j Q v$$

Normierte Impedanz

$$\frac{Y}{G} = 1 + j \frac{Y_k}{G} v = 1 + j Q v$$

Normierte Admittanz

$$Q = \frac{P_b}{P_w} = \frac{Z_k}{R} = \frac{\omega_0 L}{R} = \frac{1}{\omega_0 R C}$$

Güte

$$Q = \frac{P_b}{P_w} = \frac{Y_k}{G} = \frac{\omega_0 C}{G} = \frac{1}{\omega_0 L G}$$

Güte

$$\varphi_{i \rightarrow u} = -\arg(Z) = -\arctan(Q v)$$

$$\varphi_{u \rightarrow i} = -\arg(Y) = -\arctan(Q v)$$

Leistung

Augenblicksleistung

$$p(t) = \frac{1}{2} U_S I_S (\cos(\varphi) - \cos(2\omega t + \varphi))$$

Wirkleistung

$$P_w = U_{\text{eff}} I_{\text{eff}} \cos(\varphi) = \frac{1}{T} \int_0^T u(t) i(t) dt$$

Scheinleistung

$$P_S = U_{\text{eff}} I_{\text{eff}}$$

Blindleistung

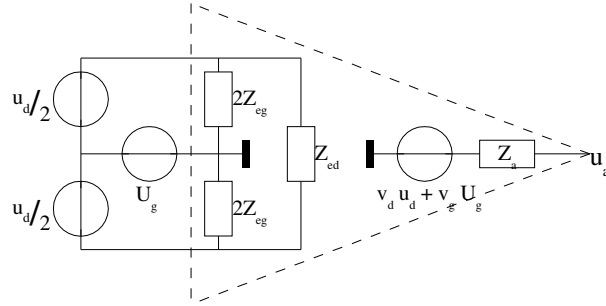
$$P_b = U_{\text{eff}} I_{\text{eff}} \sin(\varphi)$$

Operationsverstärker

Idealer OPV

$$\frac{u_a}{u_d} = \infty \quad u_d = 0$$

Realer OPV



Differenzverstärkung

$$v_d = \frac{u_a}{u_d} \Big|_{U_g=0}$$

Gleichtaktverstärkung

$$v_g = \frac{u_a}{u_g} \Big|_{u_d=0}$$

Gleichtaktunterdrückung

$$G = \frac{v_d}{v_g}$$

Differenzeingangsimpedanz

$$Z_{ed} = \frac{u_d}{i_{ed}} = \frac{R_{ed} \approx M \Omega}{1 + i \omega R_{ed} C_{ed}}$$

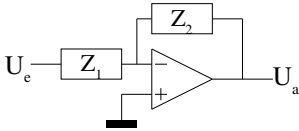
Gleichtakteingangsimpedanz

$$Z_{eg} = \frac{U_g}{I_{eg}} = \frac{R_{eg} \approx G \Omega}{1 + i \omega R_{eg} C_{eg}}$$

Ausgangsimpedanz

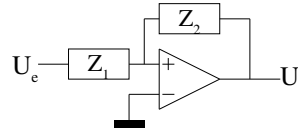
$$Z_a = \frac{u_a}{i_a} = R_a + i \omega L_a$$

Invertierender Verstärker

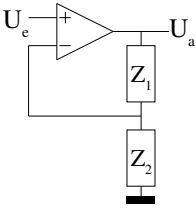


$$H(s) = -\frac{Z_2}{Z_1}$$

Nicht invertierender Schmitt-Trigger

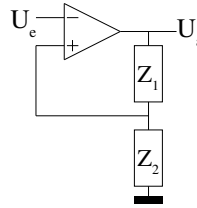


Nicht invertierender Verstärker

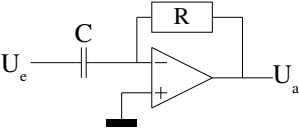


$$H(s) = 1 + \frac{Z_1}{Z_2}$$

Invertierender Schmitt-Trigger

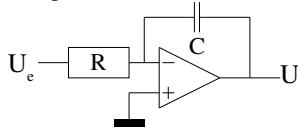


Differenzierer



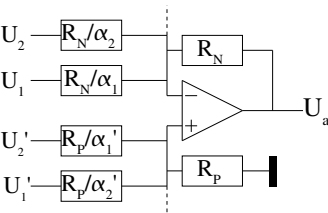
$$H(s) = -sRC = -s$$

Integrierer



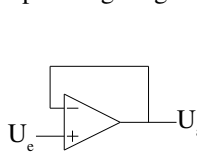
$$H(s) = -\frac{1}{sRC} = -\frac{1}{s}$$

Addierer



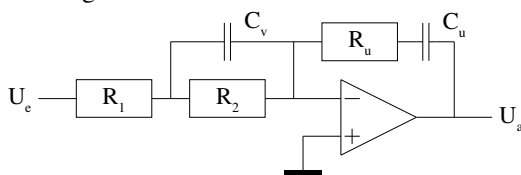
$$\sum_{i=1}^n \alpha_i' = \sum_{i=1}^m \alpha_i \Rightarrow U_a = \sum_{i=1}^n \alpha_i' U_i' - \sum_{i=1}^m \alpha_i U_i$$

Spannungsfollower/Impedanzwandler



$$H(s) = 1$$

PID-Regler



$$H(s) = -\frac{(1+sR_u C_u)(1+sR_2 C_v)}{s C_u (s R_1 R_2 C_v + R_1 + R_2)} = \frac{(1+S_1)(1+S_2)}{S_3(1+S_4)}$$

$$V = -\frac{1}{(R_1 + R_2) C_u}$$

$$T_1 = R_u C_u$$

$$T_2 = R_2 C_v$$

$$T_0 = \frac{R_1 R_2}{R_1 + R_2} C_v$$

$$K_p = -\frac{R_u C_u + R_2 C_v}{(R_1 + R_2) C_u}$$

$$K_i = -\frac{1}{(R_1 + R_2) C_u}$$

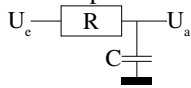
$$K_D = -\frac{R_u R_2 C_v}{R_1 + R_2}$$

$$T_1 = R_u C_u + R_2 C_v$$

$$T_D = \frac{R_u R_2 C_u C_v}{R_u C_u + R_2 C_v}$$

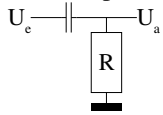
Passive Filter

RC-Tiefpaß



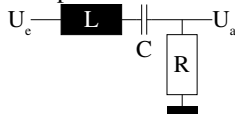
$$H(s) = \frac{1}{1+sRC} = \frac{1}{1+S}$$

RC-Hochpaß



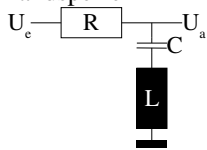
$$H(s) = \frac{sRC}{1+sRC} = \frac{S}{1+S} = \frac{1}{1+\frac{1}{S}}$$

Bandpaß



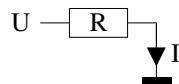
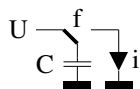
$$H(s) = \frac{sRC}{s^2LC+sRC+1} = \frac{S_1}{S_1S_2+S_1+1} = \frac{1}{1+Q\left(S+\frac{1}{S}\right)} = \frac{\Delta\Omega S}{S^2+\Delta\Omega S+1}$$

Bandsperre



$$H(s) = \frac{s^2LC+1}{s^2LC+sRC+1} = \frac{S_1S_2+1}{S_1S_2+S_1+1} = \frac{Q\left(S+\frac{1}{S}\right)}{1+Q\left(S+\frac{1}{S}\right)} = \frac{S^2+1}{S^2+\Delta\Omega S+1}$$

Switched Capacitor



$$R_{eq} = \frac{1}{Cf}$$